



(19) Europäisches Patentamt
European Patent Office
Office européen des brevets



(11) Publication number:

0 633 041 A1

(12)

EUROPEAN PATENT APPLICATION

(21) Application number: 93110531.6

(51) Int. Cl.⁶: A61N 5/10

(22) Date of filing: 01.07.93

(43) Date of publication of application:
11.01.95 Bulletin 95/02

(84) Designated Contracting States:
AT BE CH DE DK ES FR GB GR IE IT LI LU MC
NL PT SE

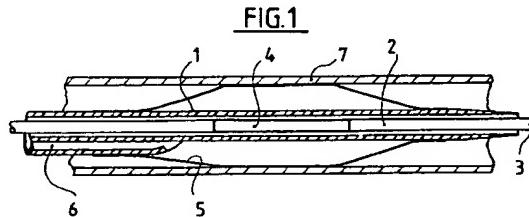
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(54) Medical appliances for the treatment of blood vessels by means of ionizing radiation.

(57) An appliance comprising a catheter 1 in which is centered a guide wire 2, a dilatation balloon 5 mounted coaxially on the catheter, and a radioactive radiation emitter in the form of a filament 4 integrated into the guide wire 2 inside the balloon 5.



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This invention relates to a medical appliance for the treatment of a portion of blood vessel by means of ionizing radiation, comprising a catheter for percutaneous transluminal treatment of the blood vessel, an inflatable dilatation balloon surrounding the catheter, a radioactive radiation emitter, and means for advancing, resp. removing, the radioactive radiation emitter into, resp. from, the portion of the blood vessel, respectively it relates to a medical appliance for the treatment of a portion of blood vessel by means of ionizing radiation, comprising a catheter defining a perfusion channel, a radioactive radiation emitter, and means for advancing, resp. removing the radioactive radiation emitter into, resp. from, the portion of the blood vessel.

Atherosclerosis causes thickening and hardening of arteries and formation of deposits of plaque or plaque-ridden tissue within the arterial lumen. Such a disease is commonly treated by means of percutaneous transluminal angioplasty techniques involving, i.a., the non-surgical widening of a passage through an artery by means of a balloon inflated to dilate the area of obstruction or the abrasion of the deposits by means of atherectomy. Unfortunately, the major limitation of these angioplasty or atherectomy techniques is the relatively important rate of restenosis. As it has been shown, the balloon angioplasty produces intimal and medial injury leading to excessive platelet aggregation and cell mediators activation followed by an elevated production of myocital growth factors. The cascade of these events, regulated by arterial wall cells nuclei, results in hyperproliferation of smooth muscle cells and migration of myocytes and macrophages from the media layer towards the intima and further accelerates excessive neo-intimal formation leading to lumen narrowing. Many approaches to prevent this phenomenon have been tested, among which regimes of anticoagulation, antiplatelet therapy, vasodilators, and serum cholesterol level reducers, however, without appreciable therapeutic effect. As a further approach to this problem, it has been found that ionizing radiation could prove helpful in the treatment of unwanted cell proliferation which causes recurrent stenoses or occlusions after angioplasty.

The document International Journal of Radiation Oncology Biology Physics, Vol. 24 Suppl. 1, page 171, which reports Proceedings of the 34th Annual ASTRO Meeting of November 1992, refers to a study on the prophylaxis of intimal hyperplasia after stent implantation in peripheral arteries using endovascular irradiation. This study was directed to the frequency of recurrent stenoses or occlusions following stent implantation in peripheral arteries due to rapid intimal hyperplasia. To stop the proliferation of connective tissue an endovascular

5 brachytherapy treatment was performed after percutaneous transluminal angioplasty. The method describes stent implantation after recanalization done by percutaneous transluminal angioplasty, and placing of a 10 Ci Iridium gamma irradiation source into the implanted stent. No specific measures are described which would ensure circumferentially uniform radiation impact on the vessel wall. In this study the radial position of the irradiation source inside the stent was determined by gravity.

10 The document JACC Vol. 21 N° 2, February 1993 : 185A, reports a study of the effects of locally delivered ionizing radiation on the proliferation response to balloon overstretching injury. The injury model was balloon angioplasty of the central artery of the ear of rabbit and the ionizing radiation was delivered as high energy beta from a sealed Sr⁹⁰ source in a single dose (skin dose of 900 rad) after a scheduled time delay from the injury. The document further refers to a second protocol using a porcine coronary injury model with trans-luminal intravascular irradiation. This publication does not disclose any specific measure to ensure an evenly distributed radiation in the vessel.

15 US Patent N° 5147282 discloses a manual irradiation loading apparatus particularly suitable for intrabronchial and gynecological irradiation treatment. The apparatus comprises a lead or equivalent radiation shielding body with a longitudinally extending cable-receiving passage therein. A cable having radioactive seeds provided on one end thereof is received in the cable-receiving passage. During storage, the portion of the cable bearing the radioactive source is located in the cable-receiving passage within the shielding body. During use, a catheter placed in a patient is joined to the shielding body and the portion of the cable bearing the radioactive source material is advanced through the cable receiving passage in the shielding body and into the catheter. The radioactive seeds are slidingly positioned inside the catheter, however the radial position of the catheter within the vessel is not controlled.

20 25 30 35 40 45 50 55 US Patent N° 4588395 describes, i.a., a catheter device for generating radioactive radiation into an artery for medicinal or repair purposes. This device comprises a catheter the tubular wall of which is collapsed at its distal end to form a sealing interface closing off the interior volume. Within this volume is located a sort of radioactive pill which can be urged forwardly by a piston connected to a flexible shaft controlled at the proximal end of the catheter, forward motion of the piston forcing the pill through the sealing interface in order to protrude from the distal end of the catheter and affect the artery. No means are provided with this catheter to secure a certain predetermined

orientation of this catheter inside the geometry of the vessel section.

In addition to irradiation external to the site, the document Wo 93/04735 also describes an apparatus for the treatment of an artery, comprising a radioactive dose and a means operatively connected to such a radiative dose to bring it into a selected region of an artery. In a first embodiment, the apparatus comprises a sheath removably positioned over a windowed housing containing a radioactive dose and connected to a catheter shaft, whereby the relative motion between catheter shaft and sheath permits moving the windowed housing in and out of the sheath, thereby exposing the radioactive dose which may affect the selected place in the artery. In a second embodiment, the device comprises a catheter shaft surrounded by an angioplasty balloon on the outer surface of which are affixed radioactive elements intended to be forced into contact with the artery wall upon inflation of the balloon. The balloon has a perfusion channel to allow perfusion of blood f.e. from proximal of the balloon to distal of the balloon. Perfusion of blood is therefore possible even during the phase when the balloon is inflated and normal blood flow is interrupted. A third embodiment, substantially similar to the first one, includes a sheath intended to provide a shielding to a radioactive dose and a motion wire to provide slidable motion of the radioactive dose within the sheath. A fourth embodiment comprises an inflatable stent delivery balloon for expansion of a stent to which a radioactive dose is associated as a cladding, a coating or an additive within the stent material itself. A fifth embodiment shows a shrinkable tubing attached to a catheter shaft and a plurality of radioactive seeds located in the tubing where they are separated from each other by heat shrinking of the tubing which therefore encapsulates the seeds.

The sheath configuration of the first embodiment suffers from the same drawbacks as the configurations known from the previously mentioned publications. The radial orientation of the radioactive dose inside the vessel is determined by gravity. In the second embodiment, the radioactive elements affixed to the balloon and forced into contact with the artery wall, the radioactive elements provide uniform radiation impact on the artery wall only as far as specifically the area of the individual radioactive element is concerned. A circumferentially uniform radiation on the artery wall is not possible with this configuration. Besides that, the radioactive elements on the outer surface of the balloon are difficult to secure on the flexible balloon surface. Their fixture would have to meet severe safety requirements against loss under all conditions. This would lead to some specific complications. Finally radioactive elements and the fixture of

these elements add unfavourably to the deflated profile of the balloon to pass through tight stenoses. The third embodiment with the slideable radioactive dose within the sheath shows the same problems as the first embodiment. It shows no means to control the transversal orientation of the sheath in the vessel. The fourth embodiment, the cladded expanding stent, represents regarding uniformity of radiation the same unfavourable situation as the configuration of the balloon with affixed radioactive elements. Finally, the fifth embodiment adds nothing to the solution of the positioning problem, it mainly refers to the problem of how to safely secure the radioactive seeds to a catheter shaft.

In all these devices, the radiation cannot be uniform, either because there is absolutely no possibility of having the radioactive element correctly positioned within the artery, or because the radioactive element irregularly bears against the vessel wall.

The document DE-3620123-A1 discloses an apparatus for measuring and irradiating body cavities which permits the placing and positioning of a light conductor at the center of a cavity in order to achieve homogeneous lighting thereof via a dispersing agent. To this effect, a light conductor is located in a tubular catheter surrounded by two optically transparent centering flexible balloons at a distance from each other and which are inflated by a dispersing agent in order to have them rest against the wall of the body cavity. The portion of the catheter which is located between the balloons is stiffer than the rest of the catheter to avoid modification of the distance between the two balloons, for instance due to curving of the catheter. The system is said to be usable for a blood vessel, but the system needs a dispersing agent and two balloons proximal and distal of the radiation source to accomodate the dispersing agent between the balloons. The two balloons are occlusion balloons. Occlusion balloons have to be resilient to safely fulfill their task in a vessel of unknown exact shape and size. Because of this resiliency, occlusion balloons can not be used simultaneously as dilatation balloons. Resilient balloons would overstretch the vessel wall when used with the higher pressures that are required for a successful angioplasty. Of course the doctor has control over the inflation pressure with resilient balloons same as with dilatation balloons, but this is not sufficient for safe angioplasty. With a resilient balloon the doctor has no control over the inflated diameter or over the shape to which the balloon is inflated.

The purpose of this invention is to improve the conditions of radioactive radiation treatment of blood vessels stenoses due to excessive intimal formation by proposing a medical appliance with

dilatation balloon or with perfusion channel for a vessel wall radiation which is uniform around the circumference of the vessel, an appliance that is simple to manufacture and easy to use, that allows traversal of narrow stenoses and that allows safe securing of the radioactive emitter to its advancing resp. removing means.

To this effect, the invention complies with the definitions given in the claims.

In that way, it becomes possible to improve dosage control of the radioactive radiation with regard to distance between the radioactive source and the vessel wall, respectively with regard to distance between radioactive source and vessel wall and timing during which the radioactive treatment has to be applied.

Specifically the essentially centered emitter ensures essentially equal radial distance to all segments of the vessel wall so that a pattern of areas with overdosage because of too narrow distance and areas with underdosage because of too wide distance to the vessel wall is avoided. The impact of radiation on the vessel wall is circumferentially essentially uniform.

If the medical appliance comprises a dilatation balloon, dilatation and radioactive treatment can be performed in one procedure. The cure for the vessel wall proliferation can be taken immediately with the cause for the vessel wall proliferation. This also has the advantage of an optimum automatic match between the location in the vessel where the cure is taken and the location in the vessel where the cause is laid. If during the procedure the dilatation balloon is not shifted inside the vessel, the radiation treatment will automatically be in the exact place where it is needed, unintentional exposure of undilated vessel portions to radiation is reduced.

If the medical appliance comprises a perfusion channel, the blood flow in the radiated vessel is not totally cut off during the time of exposure to radiation. That means, that ischemia in the areas lying in the blood flow direction behind the treatment site and the dangerous consequences of ischemia for example in coronary arteries are reduced. The radiation can with a perfusion channel be extended longer without these negative consequences and that again allows the use of an emitter with relatively low radiation density which will have less unintended side effects during the rest of the treatment procedure.

If the centered emitter is movable within the catheter, this allows specifically a quick and safe method of use for the appliance. The emitter then can be traversed to the place of treatment simply by sliding it forward inside the catheter. This ensures an easy and quick handling of the device and specifically makes sure that the vessel path from the percutaneous vessel entrance to the exact posi-

tion of the treatment place is not unintentionally overexposed to radiation due to slow advance speed of the emitter and that the exact exposure times for the radiation at the treatment site can reliably be observed. Also the vessel wall is saved from unnecessary mechanical stress from the advancement of the device. The potentially time consuming exact location of the treatment site with the medical appliance within the branched vessel system is in this case not done under radiation.

Preferably the radioactive radiating emitter is selected from the group of beta emitters. Beta emitters have a relatively short half-life. This is desirable to allow procedure times that are manageable in interventional medicine. Also the high radiation activity per specific gravity of beta emitters leads to small dimensions for the emitter which is very important in interventional techniques. Furthermore the travel distance of beta radiation inside the tissue is very short. This is very favourable for the treatment here in question. To interrupt the mechanism that lead to tissue proliferation, radiation of the surface of the vessel wall is sufficient. Radiation that travels deep into the tissue is undesirable and induces side effects. Furthermore, beta radiation needs no heavy shielding like lead or concrete. A beta radiation emitter can be shielded with plastic shieldings of practicable thicknesses so that beta emitters can be transported and handled with relatively low additional safety precautions compared to usual non-radiating products and shielded beta emitters are not bulky or heavy. Specifically the treatment room where the procedure is carried out needs no specific reinforcement in concrete, lead or other material. It is practically most important, that with the use of beta emitters the doctor can stay in the room were the treatment is made, he can directly carry out the treatment. The use of beta emitters therefore allows this treatment to be implemented in any arbitrary hospital without specific prior local precautions at the hospital itself.

The use of an emitter in form of a filament has the advantage, that the emitter can be safely fixed to the positioning means without the risk of any part of the emitter getting lost or without the risk of a container becoming untight, being thus safer than seeds or powder or other forms. In addition, a further advantage of the filament is dens concentration of dose in a small diameter.

Preferably the beta emitter is of 90 Yttrium which has a half-life of 2.7 days, a middle energy 0.942 Mev and maximal energy of 2.28 Mev, which would allow appreciable irradiation within a short distance from the filament, whereby only the internal layers of the vessel wall will be heavily irradiated while the more external structures will receive a dose which decreases with the square of the

distance. Yttrium can be made available in form of filaments, so that with the selection of Yttrium the advantages of beta emitters and of filament emitters are available.

Because of its mechanical characteristics, the filament of 90 Yttrium can have a diameter equal to or less than 0.9 mm. An emitter of this dimension is specifically suitable for percutaneous transluminal procedures.

Subject to a heat elaboration under vacuum to avoid rapid oxydation and the resulting risk of breaking, the filament of 90 Yttrium can even have a diameter equal or less than 0.2 mm. An emitter of this dimension can be introduced into the guidewire lumen of such percutaneous transluminal devices that have a very small deflated or folded profile. Such devices can use introducer sets with small outer diameter and low trauma at the percutaneous introduction site and inside the vessel such devices can cross very narrow stenoses.

If the emitter is coiled around the guide wire, this has the advantage, that an easy to accomplish and safe fixture is achieved. It can be made in a simple procedure, which is possible even under shielding conditions and thus can be made after the emitter has been activated. This is advantageous because a fixture to the guide wire before the activation of the emitter brings the problem of partially activating the guide wire together with the activation of the already affixed emitter.

Even only partly activation of the guide wire material might induce already unfavourable effects in this material, f.e. gamma radiation.

A preferred approach is to make use of a guide wire of titanium which, after activation in a powerful field of neutrons, will have a decay time of 5.8', and will advantageously solve the problem of undesirable long living of isotopes induction in other guide wires while providing mechanical qualities equivalent to those of stainless steel. Therefore with a titanium wire as carrier for the emitter, the emitter can be affixed to the carrier before the emitter is activated without any practical risk of radiation pollution. This brings the great advantage that the affixing procedure can be made under normal conditions without any radioactive shielding for the involved persons. Also in this configuration the emitter needs not to be separated again from the guide wire for reactivation of the emitter when the activity of the emitter is consumed.

These and other objects will become readily apparent from the following detailed description with reference to the accompanying drawings which show, diagrammatically and by way of example only, six embodiments of the invention.

Fig. 1 is an axial cut of the first embodiment.

Fig. 2 is an axial cut of the second embodiment.

Fig. 3 is an axial cut of the third embodiment.
Fig. 4 is an axial cut of the fourth embodiment.
Fig. 5 is an axial cut of the fifth embodiment.
Fig. 6 is an axial cut of the sixth embodiment.

5 In all the embodiments shown only the portions which have to be located in a blood vessel stenosis have been depicted; the other portions of the embodiments shown may be devised as currently practised in the art. Similarly, no particular shielding equipment for storage and transit of radioactive materials is being discussed here, reference being solely made in this respect to known techniques such as for instance those described in US Patent N° 5147282.

10 The first embodiment of Fig. 1 comprises a flexible catheter tube 1 in which is centered a guide wire 2 with a tip 3, said guide wire being in sliding fit within the catheter tube 1. A substantially cylindrical dilatation balloon 5 is mounted coaxially on the catheter tube 1 to which it is affixed annularly by its ends. The catheter 1 is a two lumen catheter in which the second lumen 6 acts as an inflation tube for the balloon 5. This balloon 5 is shown in inflated condition at the location of a 15 stenosis (not shown) of a blood vessel 7, for instance a coronary artery. A radioactive radiation emitter in the form of a filament 4 is integrated into the guide wire 2 inside the balloon 5, this radioactive filament 4 being thus essentially centered in the balloon at the location of its dilatation in the blood vessel. The radioactive radiation of the filament 4 is thus applied uniformly to the dilated stenosis due to the centering achieved by the sole dilatation balloon 5, which would result in optimal dosimetric homogeneity of the irradiation procedure. The term essentially centered for the position of the emitter inside the balloon or inside the blood vessel is used in this document to describe configurations which in normal use do not lead to alternating segments along the vessel wall circumference with unsufficiently treated cell proliferation on one side and unnecessary radioactive overdosage on the other side. This use of the term essentially centered therefore includes configurations in which the emitter in use is secured in a predetermined position in the vessel section and in which this position is spaced from the vessel wall but in which the emitter is not held in the precise center of the medical device or the vessel section but is held somehow decentered and in which despite of such decentralisation of the emitter, the treatment results that are achieved with the device are still satisfactory from a medical point of view.

20 25 30 35 40 45 50 55 The embodiment of Fig. 2 comprises the basic configuration of the first embodiment of Fig. 1 with an added perfusion capacity via holes 8 and 9 respectively arranged in the wall of the catheter 10 before and after the balloon 5. The radioactive

filament 40 is affixed to the distal end of the guide wire 2. In addition to the balloon centering and resulting uniform irradiation achieved by the embodiment of Fig. 1, this embodiment permits maintaining the irradiation for a substantially longer time as blood flow is no more hindered by the balloon. It also permits to place the radioactive emitter at the level of angioplasty without getting the distal part of the guide wire out of the catheter.

The embodiment of Fig. 3 combines the basic configurations of the embodiments of Figs. 1 and 2 except that in this embodiment the filament 45 is coiled around the guide wire 2 to facilitate assembly thereof.

The fourth embodiment of Fig. 4 comprises a flexible catheter tube 11 in which is centered a guide wire 21 with a distal tip 3, said guide wire 21 being in sliding fit within the catheter tube. This catheter tube 11 comprises at its distal end a truncated cone head 16 having a rear rest shoulder 17 adapted to house the fore end of a tube 18 mounted in sliding fit over the catheter 11. This tube 18 is adapted to enclose and free by its relative motion with respect to the catheter the flexible bristles 14 of a brush coaxially mounted on and affixed to the catheter 11. Inside the catheter 11, at the location of the bristles 14, the guide wire 21 is interrupted and its two portions are interconnected by a tube 15 coaxial to the guide wire and in which are located radioactive seeds 41. By this configuration, upon introduction of the catheter 11 into a blood vessel 7 such as, for instance, a coronary artery, and backward motion of the tube 18 with respect to the catheter 11, the bristles 14 are freed and come to rest against the inner wall of the blood vessel, thereby centering the catheter 11 into the blood vessel. The radioactive radiation of the seeds 41 is thus uniformly applied to the vessel wall and timing of irradiation can be selected at will in view of the blood flow through the bristles. Upon forward motion of the tube 18 over the catheter 11, the bristles 14 are applied against the catheter 11 which can be then easily removed from the blood vessel.

The embodiment shown in Fig. 5 comprises a flexible catheter tube 13 with a guide wire 2 centered in sliding fit therein as in the previous embodiments. The catheter 13 comprises a series of apertures 23 regularly spaced all around its distal portion and the inner channel of the catheter tube 13 is fed at its proximal end by a source of physiological solution under pressure (not shown). Inside the catheter tube, in the region of the apertures 23, a radioactive radiation emitter 46 in the form of a coiled filament is affixed to the distal portion of the guide wire 2. By this configuration, once the catheter has been introduced into a blood vessel 7 such as for instance a coronary artery, the

source of physiological solution is activated, thereby feeding the inner channel and apertures 23 of the catheter 13. The physiological solution exits by the apertures 23 and creates a uniform jet pressure all around the catheter bumping against the vessel wall, thereby assuring centering of the catheter into the blood vessel. The radioactive radiation of the filament is thus uniformly applied against the vessel wall while blood flow is assured around the catheter, thereby permitting selection at will of irradiation time. As for the embodiment of Fig. 2, the assembly of the radioactive emitter at the distal end of the guide wire permits treatment without getting the distal part of the guide wire out of the catheter.

In the embodiment of Fig. 6 the catheter is formed of an end piece 24, a tubular conduit 25 at a distance from the end piece 24, a braided self expandable temporary stent 30 having one end affixed to the end piece 24 and the other end affixed to the tubular conduit 25, a tube 26 coaxial to and sliding over the tubular conduit 25 to enclose and free the self expandable stent 30. Inside the end piece 24 and the tubular conduit 25 is centered a guide wire 2 in sliding fit therein and a radioactive radiation emitter in the form of a filament 47 is coiled around the guide wire within the area occupied by the stent 30. For introduction into a blood vessel or coronary artery, the tube 26 is pushed over the stent 30 up to the end piece 24 thereby achieving collapse of the stent 30 over the guide wire 2. Once the stent is in the selected location in the vessel, the tube 26 is pulled back towards the proximal end of the system, thereby freeing the stent 30 which comes at rest against the wall of the vessel 7. The catheter is thus centered in the blood vessel and the radiation of the radioactive filament is uniformly applied to the vessel wall while the timing of irradiation may be selected at will because of the continuing blood flow through the braiding of the stent.

In all the embodiments of Figs. 4 to 6, the radioactive treatment can be performed at any stage of the development or treatment of a stenosis, that is to say before or after balloon angioplasty or atherectomy because of the low profile of the system allowing penetration and centering even in narrowed vessels.

In all the embodiments shown, the guide wire and radioactive emitter may be fixed to the catheter instead of being movable within the catheter. As a further development, the catheter may comprise a guide wire for conventional entry into the blood vessel and the radioactive radiation emitter may be a filament affixed to or coiled around a wire intended to replace the said guide wire.

The radioactive radiation emitter can be under any appropriate form as described. Filaments will

be however preferred because they can be safely fixed to the positioning means without the risk of any part of the emitter getting lost or without the risk of a container becoming untight, being thus safer than seeds or powder or other forms. In addition, a further advantage of the filament is dens concentration of dose in a small diameter.

The radioactive radiation emitter can be selected at will, preferably however among beta emitters with a relatively short half-life, optimal penetration characteristics in tissue, and with a high radiation activity per specific gravity of the emitter (Bq/mg/mm³).

More specifically, a preferred choice will be a filament of 90 Yttrium which has a half-life of 2.7 days, a middle energy 0.942 Mev and maximal energy of 2.28 Mev, which would allow appreciable irradiation within a short distance from the filament, whereby only the internal layers of the vessel wall will be heavily irradiated while the more external structures will receive a dose which decreases with the square of the distance. Because of its mechanical characteristics, the filament of 90 Yttrium can have a diameter equal to or less than 0.9 mm. Subject to a heat elaboration under vacuum to avoid rapid oxydation and the resulting risk of breaking, the filament of 90 Yttrium can even have a diameter equal or less than 0.2 mm.

As described, the filament may be coiled around a guide wire or otherwise affixed to the guide wire in order to be integrated therewith. Accordingly, the filament may be for example welded to the guide wire.

A preferred approach is to make use of a guide wire of titanium which, after activation in a powerful field of neutrons will have a decay time of 5.8', and will advantageously solve the problem of undesirable long living of isotopes induction in other guide wires while providing mechanical qualities equivalent to those of stainless steel. In this environment, the filament will be either straight and affixed to the guide wire or coiled around the wire.

Although the balloon of the embodiments of Figs. 1 to 3 has been shown and described as being substantially cylindrical, coaxial to the catheter, and annularly affixed by its ends to the catheter, other known shapes and catheter fixing for the balloon are possible. Also, the balloon may not be coaxial to the catheter, in which case the catheter will provide for the necessary shifting of the radioactive radiation emitter to assure its essential centering inside the balloon.

Claims

1. A medical appliance for the treatment of a portion of blood vessel by means of ionizing radiation, comprising a catheter for percuta-

- neous transluminal treatment of the blood vessel, an inflatable dilatation balloon surrounding the catheter, a radioactive radiation emitter, and means for advancing, resp. removing, the radioactive radiation emitter into, resp. from, the portion of the blood vessel, characterized by a radioactive radiation emitter (4, 40, 45) essentially centered inside the balloon (5) at the location of dilatation thereof in the blood vessel.
2. A medical appliance for the treatment of a portion of blood vessel by means of ionizing radiation, comprising a catheter defining a perfusion channel, a radioactive radiation emitter and means for advancing, resp. removing the radioactive radiation emitter into, resp. from, the portion of the blood vessel, characterized by means (5, 14, 23, 30) for essentially centering the emitter (40, 41, 45, 46, 47) in the portion of blood vessel.
 3. A medical appliance according to claim 2, wherein the catheter (10) is surrounded by an inflatable dilatation balloon (5).
 4. A medical appliance according to any preceding claim, wherein the radioactive radiation emitter (4, 40, 41, 45, 46, 47) is movable within the catheter (1, 10, 11, 13, 24-30).
 5. A medical appliance according to any of claims 1, 3, 4, wherein the balloon (5) is coaxial to the catheter.
 6. A medical appliance according to any of claims 1, 3, 4, 5, wherein the balloon (5) is substantially cylindrical and annularly affixed by its ends to the catheter.
 7. A medical appliance according to any of claims 1, 3, 4, 5, 6, wherein the catheter (10) comprises a perfusion channel connected to openings (8, 9) in the catheter wall before and after the balloon (5).
 8. A medical appliance according to any of claims 2 and 4, wherein the catheter (11) is surrounded by a brush with flexible bristles (14), and wherein an outer tube (18) is mounted in sliding fit on the catheter to enclose and free the bristles of the brush.
 9. A medical appliance according to any of claims 2 and 4, wherein the catheter (13) comprises an inner channel provided with a plurality of lateral apertures (23) regularly spaced around the catheter, and wherein said inner

- channel is fed by a physiological solution under pressure.
10. A medical appliance according to any of claims 2 and 4, wherein the catheter comprises a self expandable temporary stent.
11. A medical appliance according to any of claims 2, 4, 10, wherein the catheter comprises an end piece (24), a tubular conduit (25) at a distance from the end piece, a braided self expandable temporary stent (30) having one end affixed to the tubular conduit (25) and the other end affixed to the end piece (24), and a tube (26) coaxial to and in sliding fit with said tubular conduit (25) for enclosing, resp. freeing, the self expandable temporary stent (30).
12. A medical appliance according to any preceding claim, wherein the catheter is a catheter for percutaneous transluminal angioplasty.
13. A medical appliance according to any preceding claim, wherein the radioactive radiation emitter (4, 40, 41, 45, 46, 47) is a beta radiation emitter.
14. A medical appliance according to any preceding claim, wherein the radioactive radiation emitter (4, 40, 45, 46, 47) is a filament.
15. A medical appliance according to claim 13 or 14, wherein the radioactive radiation emitter (4, 40, 41, 45, 46, 47) is of 90 Yttrium.
16. A medical appliance according to claim 13, wherein the radioactive radiation emitter (4, 40, 45, 46, 47) is a filament of 90 Yttrium with a diameter equal to or less than 0.9 mm.
17. A medical appliance according to claim 13, wherein the radioactive radiation emitter (4, 40, 45, 46, 47) is a filament of 90 Yttrium which is heat elaborated under vacuum.
18. A medical appliance according to claim 16 or 17, wherein the filament has a diameter equal to or less than 0.2 mm.
19. A medical appliance according to any preceding claim, wherein the catheter comprises a guide wire (2) in sliding fit therein, and wherein the radioactive radiation emitter is a filament (4, 40, 45, 46, 47) affixed to said guide wire.
20. A medical appliance according to any of claims 1 to 18, wherein the catheter comprises a guide wire (2) in sliding fit therein, and
- 5 21. A medical appliance according to any of claims 1 to 18, wherein the catheter comprises a guide wire in sliding fit therein, and wherein the radioactive radiation emitter (4, 40, 45, 46, 47) is a filament affixed to a wire intended to replace the said guide wire.
- 10 22. A medical appliance according to any of claims 1 to 18, wherein the catheter comprises a guide wire in sliding fit therein, and wherein the radioactive radiation emitter (45, 46, 47) is a filament coiled around a wire intended to replace the guide wire.
- 15 23. A medical appliance according to any of claims 19 to 22, wherein the radioactive radiation emitter is a filament affixed to a wire of titanium.
- 20 24. A medical appliance according to any of claims 19 to 22, wherein the radioactive radiation emitter is a filament coiled around a wire of titanium.
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- 55
- wherein the radioactive radiation emitter is a filament (45, 46, 47) coiled around the said guide wire.

FIG. 1

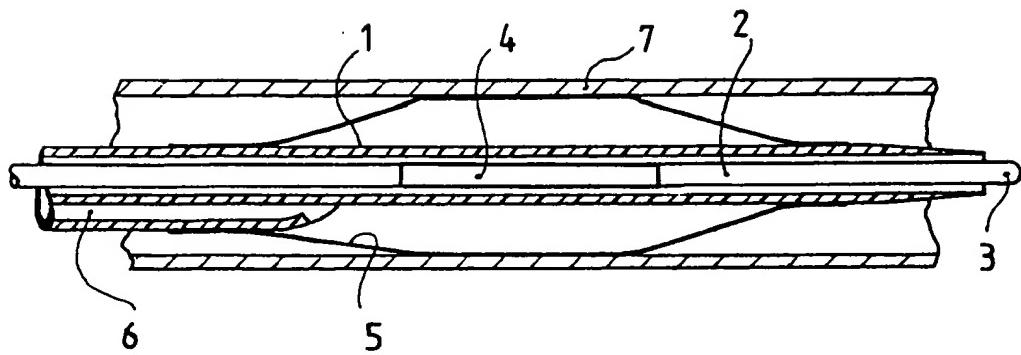


FIG. 2

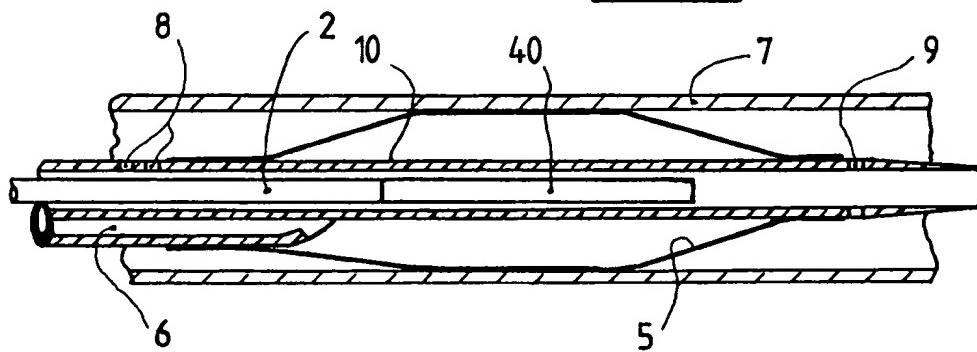


FIG. 3

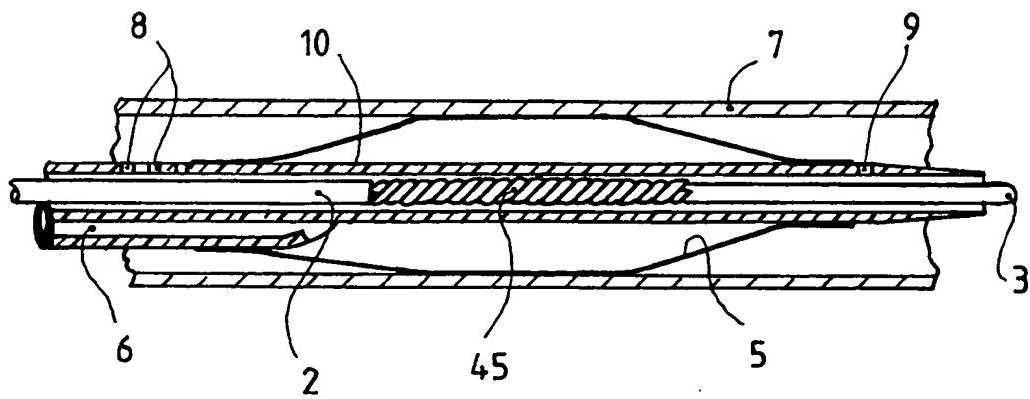


FIG. 4

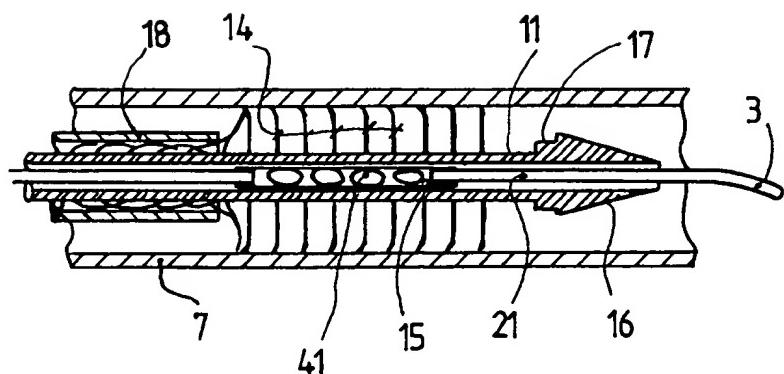


FIG. 5

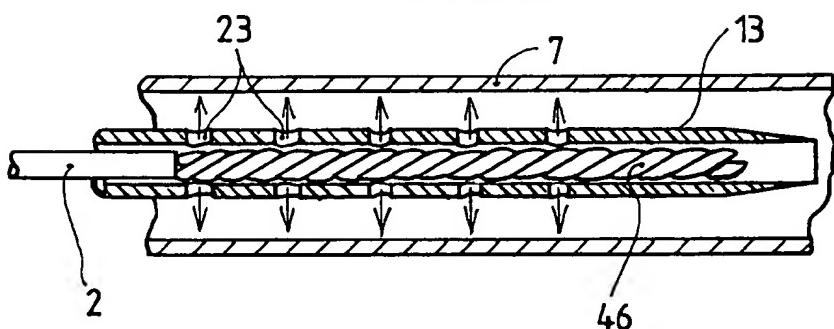
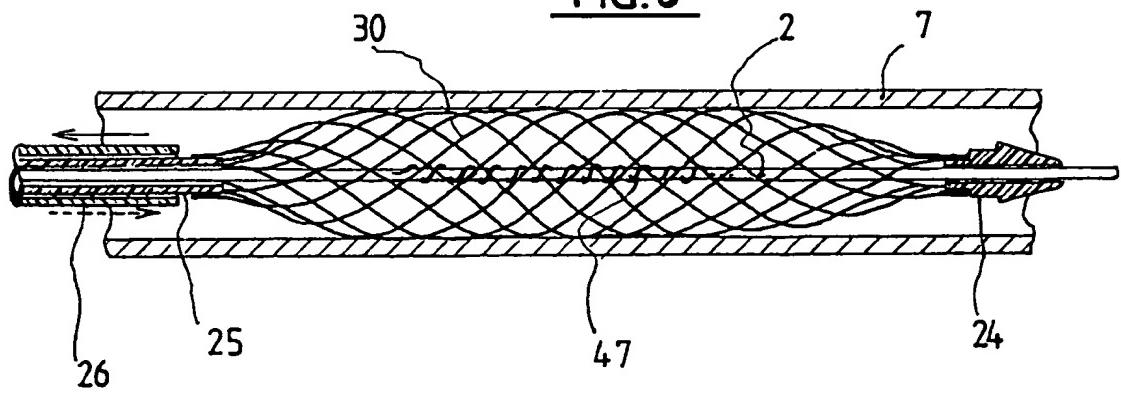


FIG. 6





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EUROPEAN SEARCH REPORT

Application Number
EP 93 11 0531

| DOCUMENTS CONSIDERED TO BE RELEVANT | | | | | | | | | |
|--|--|-------------------|--|-----------------|----------------------------------|----------|-----------|------------------|-------------|
| Category | Citation of document with indication, where appropriate, of relevant passages | Relevant to claim | CLASSIFICATION OF THE APPLICATION (Int.Cl.6) | | | | | | |
| X | DE-U-91 02 312 (WEIKL, MERKEL) * page 6, line 35 - page 7, line 20; figure 2 * | 1,4-6, 13,14 | A61N5/10 | | | | | | |
| A | --- | 2,3,12, 20,21 | | | | | | | |
| A | US-A-5 106 360 (ISHIWARA, HATTA, ABE) * column 3, line 23 - line 57 * * column 9, line 47 - line 61; figures 1,2,17 * | 1-3,5,6, 10 | | | | | | | |
| A | EP-A-0 447 745 (ISOTOPEN-TECHNIK DR. SAVERWEIN) * column 4, line 24 - column 5, line 30; figures 1,2 * | 1,2,10 | | | | | | | |
| A | GB-A-793 158 (RUMMERT) ----- | ----- | | | | | | | |
| TECHNICAL FIELDS SEARCHED (Int.Cl.6) | | | | | | | | | |
| A61N | | | | | | | | | |
| <p>The present search report has been drawn up for all claims</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 33%;">Place of search</td> <td style="width: 33%;">Date of completion of the search</td> <td style="width: 33%;">Examiner</td> </tr> <tr> <td>THE HAGUE</td> <td>30 November 1993</td> <td>Herbelet, J</td> </tr> </table> | | | | Place of search | Date of completion of the search | Examiner | THE HAGUE | 30 November 1993 | Herbelet, J |
| Place of search | Date of completion of the search | Examiner | | | | | | | |
| THE HAGUE | 30 November 1993 | Herbelet, J | | | | | | | |
| CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document | | | | | | | | | |
| T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document | | | | | | | | | |

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